Killingworth Heat Network Feasibility Study

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EXECUTIVE SUMMARY

This report presents the findings of the Killingworth Heat Network Feasibility Study. The study is funded by the department for Business, Energy, and Industrial Strategy (BEIS) and North Tyneside Council. This study should form a key part of the overall CO2e reduction and heating strategy for the Killingworth area.

Energy Demand and Supply

The Killingworth area heat demand was assessed and calculated as 70.4 GWh. Of this demand an estimated 27.4 GWh would be viable for connection to a district heating network. Key heat demands come from the council buildings, specifically the NTC Killingworth Site, 6 local schools and community centres. As well as high density social housing sites near the main network route. Key private heat demands include Morrisons and Matalan/Home Bargains in the main shopping area. One large development was identified as a key connection as the network is built out.

The majority of the heat demand is made up of existing buildings, and their owners/operators will be exploring options to decarbonise their heating systems over the next 10 years. Delivering a reliable operational district heat network will be crucial to enable these stakeholders to decarbonise their heating supply.

Heat pumps, waste heat, biomass and CHP technologies were assessed as options to supply potential heat networks. Key potential source of renewable heat identified is water source heat pumps (WSHPs) using local coal mines as the water supply.

The network is reliant on suitable energy centre locations being secured. In discussion with North Tyneside Council officers, the preferred energy centre location is the Killingworth Depot site. The site is ideally located as it sits directly above 4 potential mine seams. Following consultation from the Coal Authority the energy centre site is likely to be a suitable location to abstract and re-inject mine water. However, the available flow rate and temperatures from the mines require further investigation.

Network Assessment

The network was assessed over three phases. Phase 1 connections have been assessed as low risk connections, they include existing council buildings, social housing clusters located close to the main network spine and large commercial connections in Killingworth town centre. Phase 2 extends to connect larger connections in the northern industrial site as well as Burradon School and the adjacent social housing cluster. Phase 3 includes long term planned housing development at Killingworth Lane and the high density social housing clusters near to this development.

The DH network will be developed over three phases (see below):

Economics

A techno-economic model (TEM) was developed to assess the viability of the proposed network. The key parameters for the TEM include:

- Annual heat demand, kWh
- Peak heat demand, kW
- Energy centre tariffs
- Heat sales tariffs
- Scheme capital costs

- Operational and replacement costs
- Carbon savings /emissions vs a BAU case
- Grant funding

The 40-year economics and carbon savings for each phase of the network are summarised below:

The economics of the Phase 1 heat network return a low IRR and therefore would require grant funding to be viable from a local authority's perspective, which is available through the planned Green Heat Network Fund (GHNF).

Grant funding

Green Heat Network Fund is a £288m fund available to support heat network project with capital grants available to up to but not including 50% of the project capex.

The grant funding core requirements are shown below with the results from the preferred option:

Key Sensitivities and Risks

Key sensitivity parameters for the prioritised network areas include:

- Capital costs
- Network heat demand and key sites not connecting
- Energy tariffs including heat sales tariffs, energy centre fuel purchase tariffs and indexation of energy tariffs
- Grant funding

The key risks for the project are:

- Confirming the water availability from the mines below the identified energy centre site
- Achieving grant funding for the Phase 1 heat network

Commercial and Governance Issues

The primary objectives for the project are to maximise CO2e savings, provide affordable heat to residents and businesses. The overall return on the investment is low, therefore the schemes will need to be either public sector led or led by companies who can take a longer-term view. If grant funding is secured then there is the possibility that the network will meet the investment criteria of more private sector companies.

Next Steps

If the project is to be progressed, the next steps include:

- Securing commitment to the project from North Tyneside Council members
- Safeguard land at Killingworth Site for energy centre
- Continued engagement with the Coal Authority to develop:
	- o Technical viability of utilising mine water from the proposed energy centre location
	- o Available flowrates and temperatures
	- o Confirm abstraction and reinjection locations
	- o Commercial structure of heat supply
- Engagement with potential network connections and re-assess proposed network phasing
- Engagement with Northumberland Estates about development at Land Off Killingworth Lane
- Liaise with planning department to gather more detail on future planned developments
- Further engagement with Northern PowerGrid to determine cost of connection and available capacity
- Engagement with GHNF team to fully understand requirements and ensure a robust grant funding bid is submitted

1 INTRODUCTION

1.1 General

This report presents the findings of the Killingworth Heat Network Feasibility study. The project is supported by Heat Networks Delivery Unit (HNDU) from the Department for Business, Energy, and Industrial Strategy (BEIS). The work has been conducted by Sustainable Energy (SEL).

1.2 Project Scope

We were commissioned to undertake a feasibility study for Killingworth Township. The scope of the feasibility study included:

- Update predicted annual energy demands and profiles for heat and, if required, electricity and cooling
- Compile an energy demand database that includes building type, peak demand, annual demand and hourly profiles for all existing and planned buildings
- Identify potential energy centre / substation locations, considering locations of low and zero carbon plant and / or peak and reserve boilers and present the risks and benefits associated with each
- Compile energy demand and supply and risk assessments in line with latest information from development plans, planning applications, energy centre land availability assessment update, site surveys and any other relevant sources (including achieving sufficient accuracy of peak heat demands and annual heat consumptions)
- Identify electricity and gas capacity requirements for energy centres and decentralised options and provide budget connection costs
- Determine plant requirements and sizing (in line with likely grant funding requirements) including arrangements for peak and reserve boilers, thermal and electrical storage and potential for power supply
- Confirm feasible routes for heating/cooling pipes and power cables and suitable locations for building connections (liaising with local Highways, Structural and Planning teams to obtain critical feedback on proposed routes)
- Assess network temperatures including low temperature hot water and ambient network options
- Provide energy and mass balances (within the techno-economic model) using tried and tested in-house software to dynamically model hourly energy supply in response to hourly demand
- Provide a phased approach that includes detailed futureproofing considerations
- Provide heat demand sensitivity assessment that considers relevant and specific factors such as likely changes to planned developments and changes in occupancy for existing buildings (in light of C-19 or anything else) as opposed to a nominal percentage variation
- Review heat and power supply technology selection considering factors including, but not limited to, changes to energy price, CO2e, CAPEX and OPEX forecasts
- Compare net present cost of all potential centralised and decentralised options to provide an appropriate economic comparison that assesses whole life costs
- Develop network hydraulic models using specialist design software
- Confirm demand assessment assumptions
- Confirm energy centre location options
- Assess connection risk
- Assess risk associated with energy centre location and identify mitigation measures and information required for energy centre planning application
- Complete optimisation and a concept design for preferred option:
- Energy centre plant (RIBA stage 2)

- Network spine and branches (RIBA stage 2)
- Domestic and commercial (design of HIUs and substations to RIBA stage 2)
- Undertake techno-economic modelling to assess and optimise options
- Compare potential options to business-as-usual case or counterfactual to determine the economics and compare risks, issues, benefits and disbenefits
- Develop an investment timeline delivery plan to confirm the network delivery strategy to include a long-term phased delivery strategy (to be agreed with Client) which outlines phasing of network development, timeline for connection of buildings / clusters and integration of future heat supply sources
- Identify funding gaps that could be supported through Green Heat Network Fund
- Assess the annual and lifetime carbon impact of all network options
- Assess how parameters such as development costs, CAPEX, OPEX, connection charges, developers' contributions, economic value of CO2e savings impact scheme viability
- Undertake meetings and workshops with Client to establish project priorities, critical success factors, hurdle rates and appetite for risk
- Identify next steps and implementation requirements for the recommended scheme

All work is compliant with the HNCoP, and we considered UK and international best practice.

1.3 Project Background

The council recognise a number of potential opportunities associated with the provision of lower cost, lower carbon energy which could arise from a district heat network in the Killingworth area and wishes to further explore such opportunities. This specific piece of work progresses initial heat mapping and master planning results for the area of Killingworth the council has undertaken in 2015. The heat mapping exercise identified six heat clusters across the North Tyneside, Killingworth Town Centre was one of those clusters and therefore Council applied for HNDU funding to conduct techno-economic feasibility study.

In 2019 NTC declared climate emergency and set a plan to be carbon net zero emission by 2030. Decarbonisation of heat is a key challenge in achieving net zero carbon.

The North East Local Partnership (NELEP) Energy Accelerator programme was designed to support Local Authorities like North Tyneside Council and help low carbon and energy efficient projects become a reality. NELEP offers expertise, capacity and funding to NTC associated with this study.

1.4 Project Drivers

The councils' key drivers for investigating heat networks include:

- Reducing carbon emissions
- Stimulating economic development
- Reducing Council operating costs using its operational buildings as anchor loads
- Addressing domestic fuel poverty
- Improving energy security

2 DATA COLLECTION

This section describes the potential customer and stakeholder engagement that has taken place. Stakeholder engagement is critical to developing successful energy networks and the engagement work carried out to date will need to continue if the project progresses through to subsequent HNDU stages of development.

A data collection exercise was undertaken to enable the revision of energy mapping of existing and future energy demands as well as potential energy sources, barriers and constraints. As part of this process, the energy demand assessment area was reviewed and amended to include land off Killingworth Lane which extends to the northeast of the Killingworth Town area.

Key stakeholders were consulted to inform the data collection exercise including representatives from the NTC, HDNU, and NELEP, as discussed in section 2.2.3

2.1 Network Assessment Area

The Killingworth network assessment area was reviewed to identify areas where it could be extended.

Following consultation with the project team, planned developments to the northeast of Killingworth shall be included in the assessment and the boundary has been expanded further, as shown i[n Figure](#page-17-0) 1.

Figure 1: Network Assessment Area

2.2 Identification of Potential Customers

2.2.1 Planned Developments

Planned developments may provide significant energy demands and potentially lower risk of connecting than privately owned existing sites. However, there are risks associated with energy mapping and basing network assumptions around planned developments, these include:

- Permitted developments not being built
- Changes to the density, scale and timing of planned developments

Conversely, there may be potential for the density of developments to increase, meaning that higher heat density could improve the viability of networks. [Figure 2](#page-18-0) shows planned developments identified within the Killingworth area. Further details of these are in [Table 1.](#page-18-1) Risks are considered further in section [10.3.](#page-94-1)

Figure 2: Killingworth planned developments

| Map ref. | Name | Revised Name | Details of development | Timing | Assessed further |
|-------------|--|-------------------------------------|---|-------------------|-------------------------|
| | Site 7C Mylord Crescent Camperdown Industrial Estate | Agua Leisure Developments Ltd | Change of use of an industrial building (B2/B8) to a mixed-use scheme comprising office (B1), | $\qquad \qquad -$ | Yes |

Table 1: Current information for planned developments

The heating strategy for the planned developments is currently unknown. It is unlikely that these developments will be built before the proposed Future Homes Standard comes into effect which will not allow new builds to install gas boilers. If the Killingworth heat network can offer a credible alternative to installing ASHPs then there is a good possibility that they will connect. Planning policy can be used to promote and facilitate the development of district heat networks and the NTC planning team has an important role to play in developing and supporting guidance and working with developers.

2.2.2 Existing Sites

Existing sites within the assessment area were identified and their energy demands assessed. The following sites have been included in the energy demand assessment but may not connect to the network:

- Sites with annual demands below 50 MWh, unless of strategic importance
- Existing sites within planned development areas

Details of all sites identified and assessed within the energy demand assessment area are shown in [Appendix 1: Energy Demand](#page-106-1) [Assessment.](#page-106-1)

2.2.3 Engagement with Potential Key Stakeholders

Key stakeholders were identified and contact established where possible. We contacted potential stakeholders to obtain information such as development plans, energy data and tariffs, building use and occupancy levels and patterns. Information requests were presented to stakeholders by email and, where possible, via video calls.

A summary of information received from the data collection exercise for potential key network customers can be seen in [Table](#page-20-0) 2.

Table 2: Summary of engagement with key stakeholders

3 ENERGY DEMAND ASSESMENT

3.1 Energy Demand Profiles

Energy demands for potential network connections have been assessed (this included the issue of Requests for Information (RFIs) to all stakeholders). The energy demands and profiles for the panned development were modelled to consider Objective 2.1 of the CIBSE / ADE Heat Networks Code of Practice (to achieve sufficient accuracy of peak heat demands and annual heat consumptions) and comply with Future Home Standard Part L of the Building Regulations. In line with best practice hourly annual energy demand profiles were generated using in-house modelling software which apportions demands to hourly loads over the year, considering degree day data¹, building use and occupancy. All energy loads were then identified, categorised, and mapped.

For planned development we modelled hourly profiles of heating and domestic hot water demand, normalised against degree day data from the nearest monitoring station (Newcastle). Profiles were developed using in-house software and considered building plans, site measurements, building construction and operating parameters. Peak, base load, seasonal and annual heat demands were identified.

For existing domestic dwellings, information for the house size and age of the properties was supplied by NTC. Using this data, a heat demand was calculated for each property. More information on the methodology can be found in [Appendix 2: Heat](#page-112-2) [Demand Modelling](#page-112-2) Methodology.

Where no building data was available, data derived from hundreds of in-house data collection exercises for similar buildings was utilised and a demand profile for the building was constructed using in-house software or selected from our profile database as appropriate. Relevant Building Regulations were considered for planned developments. Electricity profiles for key electricity loads were identified from half hourly data or modelled where this was not available.

For each building and network phase, the hourly heat demand model was used to identify the average, maximum and minimum hourly demand throughout the year.

3.2 Energy Demand Assessment Results

Geographic Information System (GIS) software was used to map the key heat, electricity, and cooling demands for the Killingworth area. The symbols show the site location and graduate in size according to energy demand to depict the nature of the energy loads within the heat map area. The larger the symbol, the greater the energy demand. [Appendix 1: Energy Demand](#page-106-1) [Assessment](#page-106-1) shows demands for all network connections in detail, [Appendix 2: Heat Demand Modelling](#page-112-2) Methodology shows heat demand model methodology and assumptions.

3.2.1 Heat Demand

The heat demands for all potential network connections are shown in [Figure 3.](#page-22-0) The largest commercial heat demand arises from the NTC Killingworth site. [Table 3](#page-22-1) shows details of top 5 heat demands for single sites. The total heat demand for both commercial and residential sites identified within the energy demand assessment area is approximately 70,249 MWh.

¹ Degree days are a type of weather data calculated from outside air temperature readings. Heating degree days and cooling degree days are used extensively in calculations relating to building energy consumption. They are used to determine the heating requirements of buildings, representing a fall of one degree below a specified average outdoor temperature (15.5°C) for one day.

Figure 3: Heat Demands

| Rank | Name | Ownership | Building use | Annual heat demand, MWh | Source of data |
|-------------|-------------------------------|-----------------------|---------------------|-----------------------------------|--------------------------|
| 1 | Killingworth Site | Public Sector | Office | 1,522 | Actual data (metered) |
| 2 | Matalan/Home Bargains | Private Sector | Retail | 1,277 | Estimated using data |
| 3 | Morrisons | Private Sector | Retail | 1,212 | for similar sites |
| 4 | George Stephenson High School | Public Sector | Education | 985 | Actual data (metered) |
| 5 | White Swan Centre | Public Sector | Education | 858 | |

Table 3: Top 5 commercial heat demands within assessment area

[Figure 4](#page-23-0) shows the proportion of heat demand from the site apportioned to each ownership.

Figure 4: Heat demand split by ownership

[Figure 5](#page-23-1) shows further breakdown of the heat demand by building use.

Figure 5: Categorisation of heat demand

From [Figure 4](#page-23-0) an[d Figure 5](#page-23-1) the majority of heat demand (62%) is associated with low rise private housing within the social housing clusters identified in WP1. From previous project experience it is very difficult to get engagement at scale from private sector housing and will be unlikely connect to a heat network. Therefore, the heat demand breakdown without existing private housing is shown i[n Figure 6](#page-24-0) and [Figure 7.](#page-24-1)

Figure 7: Categorisation of heat demand (excluding private housing)

3.2.2 Electricity Demands

The electricity demands have been assessed to analyse the potential for private wire connections. The total electricity demand for all identified key non-domestic electricity demands within the energy demand assessment area is approximately 19,116 MWh. The electricity demand for potential network connections are shown in [Figure 8.](#page-25-0)

Figure 8: Electricity demands

The largest electricity demands are shown in [Table 4.](#page-25-1)

Table 4: Top 5 electricity demands

Figure 9 shows the proportion of electricity demand from the site apportioned to each ownership.

Figure 9: Commercial electricity demand split by ownership

Figure 10: Commercial electricity demand split by building usage

3.2.3 Cooling Demands

Cooling demands are only assessed for connections that are likely to have or could be designed to have wet cooling systems. Within the assessment area no significant cooling loads were found.

3.2.4 Sources of Data for Energy Demand Assessment

Half hourly gas and electric data was available for all council sites in the assessment area. We attempted to establish contact with the largest potential heat demand customers in the area. However, no data was forthcoming from any of the private connections. For each of these sites the heat demand was based on similar sites and proportioned to the area of the buildings.

For residential connections a heat demand model was created as discussed in [3.1.](#page-21-0) [Table 5](#page-27-0) summarises the sources of the energy demand assessment.

Table 5: Summary of energy demand data sources

3.3 Summary

A significant proportion of the energy demands within the Killingworth area arise from low density, private sector housing (62%). Due to the difficulty in predicting uptake of a heat network connection for existing private housing, this assessment will only consider social housing connections. In the later phases of the network there is a significant planned development that could benefit the heat network. Therefore, engagement with the planners and site developers should be made a priority.

When excluding private housing, there is a significant heat demand from public sector buildings (17.4%) and social housing (36.5%).

Key potential heat network demands include NTC's Killingworth Site, Morrisons and public sector schools.

4 ENERGY CENTRE ASSESSMENT

4.1 Potential Energy Centre Locations

Figure 11:Potential energy centre locations

The preferred energy centre location was determined to be the Killingworth Depot site. This site has planning permission to demolish some of the existing buildings and would provide a substantial plot for locating an energy centre. The site is within an industrial area where large vehicle access would not be restricted. The site would also be in close proximity to one of the largest network demands, the Killingworth site.

4.2 Existing and Planned Energy Sources

Potential low carbon or renewable energy sources within or near the network assessment area were assessed to identify any energy sources that may have potential to supply a heat network.

Existing borehole records, mine entries and large water sources were assessed, and the findings are presented in [Figure 12.](#page-29-0)

Figure 12: Potential heat sources

There were no borehole records² found in the area that yielded any water. However, several mine workings have been identified that suggested there could be potential for mine water to be used as a heat source.

Mine Water Assessment

Mine water was assessed as potential energy source. [Figure 13](#page-30-0) shows seam data provided by Coal Authority. For mine water to be a suitable heat source the abstraction and reinjection boreholes need to be sufficiently separated to prevent cooling of the abstracted water. This can either be from having a long surface pipeline to increase separation or by abstracting and injecting into different interconnecting seams.

Figure 13: Mine water seams across assessment area

The preferred energy centre location sits above 4 potential seams. This would enable a minimum amount of abstraction and discharge pipework. The approximate depths of the 4 seams below the energy centre are shown in [Figure 14.](#page-31-0) The interconnectivity of the seams would need to be assessed with a further study from the Coal Authority.

² British Geological Survey: GeoIndex - [British Geological Survey \(bgs.ac.uk\)](http://mapapps2.bgs.ac.uk/geoindex/home.html?layer=BGSBoreholes&_ga=2.128162252.1739623680.1649074892-1659838812.1649074892)

Planned energy sources

No planned energy sources were identified within or near by the assessment area.

4.3 Domestic Counterfactual

Counterfactual solution is an alternative to the current heating system and would be considered as a future solution e.g., low carbon counterfactual would be individual ASHPs.

For the purpose of this study, gas boilers have been assumed as business as usual (BAU) for every connection. Counterfactual for social housing is assumed to be gas boilers to prevent customer detriment and for commercial connections and planned development individual ASHPs have been assumed as counterfactual.

4.4 Renewable/ Low Carbon Heat Source

[Table 8](#page-33-0) shows potential heat sources and network options.

4.4.1 Short list assessment

The options from the long list assessment have been assessed and have been condensed to a short list, which considers possible risks, benefits and disbenefits of the selected options. The following options have been shortlisted:

LTHW Network Options

- MWSHP DHN (se[e Figure 15](#page-35-0) and [Table 9\)](#page-36-0)
- ASHP DHN (see [Figure 16](#page-37-0) and [Table 10\)](#page-38-0)

Counterfactual

• ASHPs in each building (see Figure 17 and Table 11)

Figure 15 : Schematic of Open Loop Mine Water Heat Network

Table 9: Specific issues, risks, benefits and disbenefits for open loop MWSHP using mine water DHN

Figure 16: Schematic of ASHP Heat Network

Figure 17: Schematic of Individual ASHPs

Table 11: Specific issues, risks, benefits and disbenefits for individual ASHP

4.5 Summary

The preferred energy centre location was determined to be the Killingworth Depot site, which would utilise the mine water seams. This location was considered to be the most suited as it is on council owned land, located in close proximity to council buildings, and situated above several mine water seams. The heat source capacity would need to be determined with further analysis from the Coal Authority on available flow rates to ensure that it could supply enough heat for all identified potential connections. If the mine water capacity could not supply the full energy demand, then ASHPs could be used in conjunction with a mine water connection. The Killingworth site should have enough free space to accommodate these if required.

For this study it has been assumed that the mine water capacity will be sufficient due to the four seams located directly under the energy centre. Peak and back-up boilers would be located within the same energy centre.

5 NETWORK ROUTE ASSESSMENT

The key assumptions used for network route assessment can be found i[n Appendix 4: Network assessment.](#page-119-0) Further details on network sizing and costing can be found under the heading Network costs in Appendix 6: [Techno Economic Modelling](#page-125-0) – Key [Parameters.](#page-125-0) The results of the economic assessment are shown in section [8.6.](#page-81-0)

5.1 Heat Network Route Identification

Site terrain and land ownership, as well as any potential natural and infrastructure constraints have been assessed. The proposed network route is shown in [Figure 18.](#page-42-0)

Figure 18: Proposed network route

5.1.1 Linear Heat Density

The linear heat density of the network has been assessed to identify sections with a low linear heat density that are likely to significantly reduce the economics of the network. Route sections with a linear heat density below 3 MWh/m have been classed as low. The results of the linear heat density assessment are shown i[n Figure 19.](#page-43-0)

In the assessment area several network sections have been identified to have linear heat density of < 3 MWh/m. These are all feeds to key council buildings such as schools and areas of make up a small proportion of the network. The rest of the assessment area indicates that the network has a high potential for viability.

Figure 19: Linear Heat Density assessment

The linear heat density was assessed for the buried DHN; therefore, it does not consider the additional lengths of pipe required within parcels or development site or internally within the buildings.

Connections at the industrial park, north of Killingworth Depot were identified to have low linear heat density or higher temperature requirements therefore, the network has been optimised to include only the largest feasible connections.

5.2 Key Potential Constraints

A desktop study for the proposed network route has been undertaken and key potential network constraints were identified as shown in [Figure 20.](#page-44-0) Major natural and infrastructure constraints were found to be outside of the assessment area.

Figure 20: Key network constraints

5.2.1 Terrain

[Figure 21](#page-45-0) shows the variation in elevation across the proposed energy demand assessment area. Changes in elevation are unlikely to pose a risk to the development of a heat network or the location of the energy centre and the changes in elevation present no significant technical challenge to the pumping requirements of a district heat network.

Figure 21: Terrain constrains

5.3 Housing clusters

A large portion of the heat demand in the Killingworth area relates to residential dwellings. Details of the assessed clusters are shown i[n Figure 22](#page-46-0) and [Table 12.](#page-46-1)

Figure 22: Housing clusters

To assess which housing clusters should be connected to the network a cost benefit analysis was used to determine the network viability versus individual ASHPs.

The internal network route within the clusters depends on the housing density. If all houses in a cluster were to connect, then the network lengths per property for the different densities are:

- $High = 16.3 m/dwelling$
- $Median = 20.1 m/dwelling$
- \bullet Low = 26.5 m/dwelling

The average cost of the cluster pipework is £381/m assuming that that PEX pipework is used. The steel equivalent would be more expensive, as it only comes in 12m sections which require welding. Therefore, if all houses are connected within a cluster, then the cost per dwelling will be:

- High £6,236 /dwelling
- Medium = £8,449 /dwelling
- Low = $£10,109$ /dwelling

In the high-density clusters, we have assumed that all of the social housing within that cluster will connect but only 10% of private housing will connect. This will increase the cost per dwelling as the spine and branches (green and blue in [Figure 23\)](#page-47-0) will not reduce but the number of feeds (in red) will.

Figure 23: Cluster costing example

Therefore, the cost per dwelling for each individual cluster can be calculated based on the % split between social and private housing. The counterfactual cost of an ASHP is ~£10,000 (see sectio[n 4.3\)](#page-31-0), therefore it is more cost effective to install individual ASHPs within all, but the clusters highlighted in green below i[n Table 13.](#page-48-0)

From this analysis the only cost-effective clusters to connect are where the social housing dwellings make up at least 50% of the total dwellings. Only clusters N01, N02, N102, N106 and N204 will be considered for connection to the heat network.

5.4 Summary

The selected network route considers:

- Minimising pipe length
- Routing through publicly owned land and service areas of connected buildings as much as possible
- Trench excavation, backfilling and reinstatement costs for different ground conditions
- Physical constraints and site barriers
- The outputs of hydraulic modelling exercises (including pipe lengths, diameter, insulation, and materials)
- Calculated heat distribution losses throughout the network
- CIBSE / ADE Heat Networks Code of Practice (specifically Objective 2.5)
- Linear heat density
- Critical feedback from planners
- Planned infrastructure projects
- Liaison with DNOs, scrutiny of historical OS maps, consideration of land ownership and future developments

6 RECOMMENDED SCHEME OPTIONS ASSESSMENT

The key assumptions used in the network assessment are discussed in. [Appendix 3: Key Parameters and Assumptions.](#page-114-0) The results of the economic assessment for the preferred network option are shown in section [8.](#page-78-0)

6.1 Phasing

A detailed sizing exercise has been undertaken using SEL's heat pump and thermal sizing tool. The tool analyses the hourly network heat demand, network losses, water source temperature, heat pump capacity and modulation and thermal store size on an hourly basis for a full year taking into account hourly, daily and seasonal variation as well as peak and off-peak electricity tariffs. Further details of SEL's heat pump and thermal sizing tool are included in Appendix 5: [Technology Sizing.](#page-121-0)

The proposed network is assessed over three phases:

- Phase 1: Key existing Council owned buildings, shopping centre and social housing clusters N01 and N02
- Phase 2: Larger loads from industrial estate, social housing cluster N204 and council owned Burradon School.
- Phase 3: Long term planned developments and social housing clusters N102 and N106.

The network phases, shown in following section, have been chosen based on technical issues, economics, timing of developments and risks. The network phasing and timing has been estimated based on high level information from the North Tyneside Council to coincide with the desire to achieve Green Heat Network Funding for Phase 1 network. The timings of further phases are based on experience for the development of heat networks within city/town centres. The phasing and timing of network should be further assessed if additional details for the area become available.

Figure 24: Phased network route

6.1.1 Phase 1

Phase 1 has identified seventeen potential connections. The key Phase 1 connections include North Tyneside Council buildings, including council schools, Killingworth shopping centre including Morrisons and Matalan/Home bargains. The network route and connected buildings are shown in [Figure 25,](#page-50-0) further details on connected buildings are shown in [Table 14.](#page-50-1)

Figure 25: Phase 1 Heat Network Layout

The profiles for each phase have been created based on the identified heat demands for each connection. The heat demand profile for a year from January to December is shown in [Figure 26.](#page-51-0) [Figure 27](#page-52-0) displays the Phase 1 average, minimum, and maximum heat demand over 24 hours.

Figure 26: Annual heat demand profile for Phase 1

Notably Average kW → Maximum kW → Minimum kW → Summer month average → Winter month average

Figure 27: Average, maximum and minimum hourly heat demand for Phase 1

A summary of the Phase 1 network is shown i[n Table 15.](#page-53-0)

Table 15: Phase 1 summary

6.1.2 Phase 2

Additional to Phase 1 connections, seven potential connections have been identified as a Phase 2 heat network. The key Phase 2 connections include private sector buildings withing the Industrial Estate, social housing cluster and council owned school. The network route and connected buildings are shown in [Figure 29.](#page-53-1)

Figure 29: Phase 2 network layout

Table 16: Phase 2 network connections

[Figure 30](#page-54-0) shows Phase 2 annual heat demand profile. Average, minimum, and maximum heat demand over 24 hours for Phase 2 is shown i[n Figure 31.](#page-55-0)

Figure 30: Annual heat demand profile for Phase 2

Figure 31: Average, maximum and minimum hourly heat demand for Phase 2

Figure 32: Load duration curve for Phase 2

A summary of the Phase 2 network is shown in Table 17.

Table 17: Phase 2 summary

6.1.3 Phase 3

Two Phase 3 connections have been identified: planned development and social housing cluster. Since, social housing cluster N106 is nearby planned development it should only be connected if proposed development is brought forward and connected to the Killingworth heat network. The network route and connected buildings are shown in [Figure 33.](#page-56-0)

Figure 33: Phase 3 network layout

Table 18: Phase 3 network connections

Figure 34: Annual heat demand profile for Phase 3

Figure 35: Average, maximum and minimum hourly heat demand for Phase 3

Figure 36: Load duration curve for Phase 3

A summary of the Phase 3 network is shown in Table 19.

6.2 Prioritised Network Option

The heat demand and network assessment identified the most feasible connection for district heat network. [Figure 37](#page-59-0) shows the heat demand of the prioritised solution split by ownership. [Table 20](#page-59-1) shows further details on number of connections, ownership, and their demands

The demand for phase 1 heat is split between 27.66% of social housing and 40.88% of public sector buildings. Phase 2 demand is composed of 27.8% of social housing and 33.6% of the public sector. Phase 3 has a 24.7% public sector demand and a 27.9% social housing demand, giving NTC a high level of control over whether they connect. The proposed network is assessed over three phases.

Figure 37: Prioritised network heat demand split by ownership

Table 20: Prioritised network heat demand summary

A heat network supplied by heat pumps utilising water abstracted from Yard Seam and reinjected into the High Main Seam has been selected as the prioritised network option. However, the abstraction potential requires further assessment.

It is assumed the 2.51 MW heat pump at NTC site energy centre will serve the Phase 1 network. An additional 0.74 MW will support serving the Phase 2 network. Then additional 0.56 MW MWSHP will be installed for Phase 3. In total 3.81 MW of MWSHP will generate enough heat to serve the Phase 3 network. A summary of the network heat generation and supply is shown i[n Table 21.](#page-59-2) The key assumptions for the technology and key parameters are shown in [Appendix 3: Key Parameters and](#page-114-0) [Assumptions.](#page-114-0)

Table 21: Network summary

[Figure 38](#page-60-0) shows the hourly network heat demand ordered from highest to lowest. Heat demand below the black, blue and grey lines can be met by the heat pump(s) in each phase. The heat demand above the black, blue and grey lines is met by the thermal stores and peak and reserve boilers.

Figure 38: Load duration curve

The heat from the heat pumps will meet between 90% and 98% of the full network heat demand, including heat losses in the network. The remaining of heat demand which is not met by the low carbon technology will be met by the gas peak and reserve boilers. The peak and reserve boilers will also supply heat in the 2 weeks plant downtime a year included in the assessment for maintenance and repairs to the heat pumps.

Gas boilers were chosen as they will improve economic viability of the project due to lower gas cost against electricity. Electric boilers would also significantly increase fixed charges based on required capacity and significantly increase risk of energy centre reliance on the reliability of heat pumps (if the heat pumps are unavailable for significant periods, the operation of electric peak and reserve boilers may be an unacceptable risk for O&M contractors obligated to deliver heat at a specific price). Under the modelled assumptions the heat pumps are cheaper to operate than gas boilers and will therefore be prioritised, minimising the emissions from the energy centre.

200,000L thermal storage has been included at the energy centre to maximise the proportion of heat that can be provided from the heat pump and reduce the use of the peak and reserve gas boilers.

More details on the prioritised network option and assumptions are mentioned in section [7.](#page-65-0)

6.2.1 Energy Balance

[Figure 39,](#page-61-0) [Figure 40](#page-62-0) an[d Figure 41](#page-63-0) show the energy balance for phases 1, 2 and 3 respectively.

Figure 39: Phase 1 energy balance

Figure 40 : Phase 2 energy balance

Figure 41: Phase 3 energy balance

6.3 Summary

The proposed network has been assessed over 3 phases. Phase 1 connects key existing council owned buildings, large commercial buildings in the town centre and three social housing clusters. Phase 2 then connects larger loads from the northern industrial estate an additional social housing cluster and council owned Burradon School. Phase 3 connects longer term planned development at Killingworth Lane and a final social housing cluster.

All phases will be supplied with heat from the NTC Killingworth Site energy centre using mine water. For each phase additional mine water heat pumps will be installed to supply low carbon heat. Further assessment from the coal authority is required to confirm the potential for abstraction from the mine workings.

7 CONCEPT DESIGN

This chapter describes the scheme concept design and includes details of the primary heat sources, peak and reserve boilers, other energy centre equipment, utilities connection requirements and metering.

7.1 Futureproofing

Futureproofing measures have been considered throughout the concept design process for the network options. There is sufficient capacity in the energy centre design to accommodate further building connections, but this will need to be assessed on a case-by-case basis.

7.2 Killingworth Depot Energy Centre

The proposed energy centre utilises mine WSHPs. The backup gas boilers will be located within the energy centre building and will be used to provide heat at times of peak demand (if this exceeds the capacity of the heat pumps and thermal stores). Controls will prioritise heat from the heat pumps using thermal stores over the peak and reserve gas boilers to maximise the use of renewable technologies. A summary of the technology capacities for Phase 1 and additional requirements for Phase 2 and Phase 3 at the proposed energy centre are shown in [Table 22.](#page-65-1) [Figure 42](#page-66-0) shows process flow diagrams (PFDs) for the proposed energy centre and [Figure 43](#page-67-0) shows RIBA Stage 2 energy centre design.

Figure 42: NTC Killingworth Site PFD - Fully built out Phase 1,2 and 3

7.2.1 Energy Centre Footprint

Figure 43: NTC Killingworth Site energy centre general arrangement – Fully built out Phase 3

7.2.2 Technology Sizing

Heat Pumps

The heat pumps will be packaged units connected within the energy centre to two main circuits; the abstraction water source circuit and the primary heating circuit. The abstraction source circuit(s) operates by running a low-temperature, low pressure refrigerant fluid through a heat exchanger to extract the heat from the mine water.

The heat pump refrigerant circuit will be hermetically sealed and subject to the F-gas directive and the working fluid will be a Low Global Warming Potential refrigerant. Current refrigerant in the modelled solutions is propane (R290) with a GWP of 3. More details on disadvantages and advantages of different refrigerants can be found i[n Appendix 8: Heat pump refrigerant.](#page-130-0) In addition to the heat pump the energy centre will include heat exchanger and water treatment unit for the mine water.

The refrigerant fluid 'absorbs' the heat and boils at low temperature with the resulting gas being compressed to increase the temperature, the gas is then passed through another heat exchanger, where it condenses, releasing its latent heat to the primary heating circuit.

The heat pump capacity will be limited based on the phased network demand and the flow rate of water pumped from the mines. Consideration has also been given to the optimum balance between heat generation capacity, capital cost, maintenance costs and physical size.

A detailed sizing exercise has been undertaken using SEL's heat pump and thermal store sizing tool. The tool analyses the hourly network heat demand, network losses, water/air source temperature, heat pump capacity and modulation and thermal store size on an hourly basis for a full year taking into account hourly, daily and seasonal variation as well as peak and off peak electricity tariffs. Heat pump sizing is further assessed in Appendix 5: [Technology Sizing](#page-121-0) including further details of SEL's heat pump and thermal sizing tool. Following this exercise, a total of ~3.8 MW of mine water source heat pumps are required to serve the 3 phases.

Abstraction and reinjection boreholes

Mine water would be abstracted via an 'open-loop' system. The mine water is pumped up from the well or borehole, passed through a plate heat exchanger before being re-injected back into the mine. The mine water will have to be recirculated therefore it is important that mine workings which the boreholes abstract and reinject to are hydraulically connected. To avoid 'short circuiting' of recirculated mine water, the abstraction and reinjection boreholes are located within different seams within the same mine as shown in [Figure 44.](#page-69-0) There are potentially 4 possible seams that mine water could be extracted from as discussed in section [4.2.](#page-29-0) It is preferential to abstract from a lower seam and reinject into a higher seam as the water temperature will increase with increasing depth. This study assumes that water will be abstracted from the Yard Seam and reinjected into the High Main Seam.

Figure 44: Mine water abstraction

Peak and Reserve Boilers

The gas boilers have been sized to ensure that failure of any one item of equipment will not prevent the peak heat demand from being met. Gas peak and reserve boilers have been sized using an n+1 methodology to allow multiple boilers to modulate in unison to meet heat demands, this will provide redundancy and allow boilers to operate at their highest efficiency throughout the range.

7.2.3 Thermal Storage

Thermal storage has been included at the energy centre to maximise the proportion of heat that can be provided from the heat pump and reduce the use of the peak and reserve gas boilers. The thermal storage comprises large cylindrical, insulated water tanks which will be connected in series with each other to maximise the stratification of the stored volume. The thermal storage will be connected in parallel with the heat pump so that a proportion of low carbon heat is always used to charge the thermal stores when they are below full capacity.

7.2.4 Flues

The design of the flues needs to achieve sufficient velocity of exhaust gas to achieve adequate dispersion, avoiding concentrations of harmful gasses such as nitrogen oxides (NOx). The effects of wind loading, and structural requirements of the flues must also be assessed and incorporated into the structural design of the energy centre.

Gas boilers are expected to only operate for short periods of time and discussion with North Tyneside Counsel Air Quality manager is required. If possible, gas boiler will be ultra-low NOx versions and will run only when the network demand exceeds the capacity of the installed heat pumps and thermal stores, therefore impact on the air quality will be minimal. If required by local air quality officers, dispersion modelling can be conducted to ensure that any impact is within regulatory limits and meets local air quality objectives (and this information will be fed back into the flue design process).

Flue dispersion modelling may be required to assess the impact on surrounding buildings, including nearby tall buildings.

7.2.5 Operating Conditions

A detailed assessment of the proposed network has been undertaken and the proposed operating conditions reflect the optimal network efficiency. To ensure heat network losses are kept below 10%³, and to effectively serve a combination of new build developments and existing buildings with varying secondary systems, the heat network will need to operate variable temperature conditions.

Primary Network Temperatures

The primary heat network will provide heat via plate heat exchangers which means the flow temperature on the primary network into each building will be slightly higher at circa 85°C at peak conditions and 65°C to 75°C flow temperatures for summer conditions.

The energy generating plant in the energy centre will be made up of various technologies that have different temperature conditions that affect the efficiency of each technology (i.e. gas boilers and heat pump). Gas boilers can operate at higher temperatures of 90°C without impacting negatively on efficiency. Heat pumps, however, have a performance which is significantly impacted by the temperature conditions of the network and, to maintain effective performance, network flow and return temperatures should be as low as possible.

Controlled scheduling of heat pumps and gas boilers will be required to maintain an overall efficiency of each technology. Heat pumps will not be used to supply higher temperature peak demands, so the higher temperatures required for peak demands will be supplied by gas boilers. However, when temperatures and loads are lower (e.g. summer conditions), the heat pump will supply higher levels of demand. Detailed modelling and sizing have been carried out to consider varying demand profiles, temperature conditions and carbon impacts.

Secondary System Temperatures

The proposed network comprises mainly existing buildings and limited planned developments. It is assumed the existing buildings are currently operating at flow temperatures within a range of 80-82 $^{\circ}$ C flow and return temperatures of 60-71 $^{\circ}$ C. These buildings will require upgrades to their secondary systems and controls to make them 'district heat ready'⁴. The assessments undertaken indicate that, by replacing hot water systems and improving control for space heating systems in existing buildings⁵, target secondary side temperatures could be 70 °C flow and 45 °C return for peak conditions, and 65 °C flow and 35 °C return for summer conditions. If buildings operate at higher temperatures, then supply temperature from the heat pump needs to be higher, this has a negative impact on the SPF of the heat pump, see section [10.1.6.](#page-93-0)

Building regulations Part L Volume 1: Dwellings and Part L Volume 2: Buildings other than dwellings both require wet heating systems to be designed with a maximum flow temperature of 55°C. Any planned developments will be required to be built to these new regulations so the secondary side temperatures should be in accordance with CIBSE / ADE CP1. When connected to district heat networks, this will result in lower average return temperatures and therefore increase the efficiency of the network and the heat generating technologies. Target secondary side temperatures for planned developments should be 55°C flow and 30°C return.

³ The CIBSE/ADE HNCoP states that the calculated annual heat loss from the network up to the point of connection to each building when fully built out is typically expected to be less than 10 %

⁴ DH ready buildings have the infrastructure in place to connect to the district heat network in line with the HNCoP and other best practice

Operating Pressure

The topography of the Killingworth area has minimal height variation. The calculated static pressure required in the network will be circa 3.5 bar. Hydraulic separation will be required in high rise buildings (over 4 storeys).

The pumping pressure defines the maximum operating pressure to generate enough head to deliver the flow rate to all buildings. Hydraulic modelling was carried out to assess how the pressure in the network will vary throughout the seasons and the concept design considers maintaining maximum pressure in the system at less than 9 bar.

7.2.6 Variable Speed Pumps

The design utilises variable speed pumps in a multi-pump arrangement (3 pumps – 1no. duty, 1no. assist and 1no. standby). They will be controlled to maintain a minimum pressure difference at specific locations using index differential pressure sensors within the network. The pump set will be sequenced, and speed controlled (on a demand basis) to maintain a differential pressure that is influenced by the pressure independent control valves controlling heat demand to ensure heat demands are satisfied and flow rates are minimised.

The benefits of the variable speed function will be realised as peak flow rate conditions will typically only occur for brief periods during a heating season, with average demands being much lower.

7.2.7 Utilities Connections

A gas connection able to supply the peak and reserve boilers up to 8 MW will be required for the North Tyneside Counsel site. A budget quote was requested from Northern Gas for the North Tyneside Counsel site; however, this was not received prior to the completion of this study. An estimate figure based on similar projects has been used in the assessment.

An electricity connection able to supply the heat pumps and the energy centre will be required at with a 1.4 MVA peak capacity required at North Tyneside Council site. The budget quote from Northern PowerGrid was requested; and a budget quote of £94,422.78 (incl. VAT) was received for electrical connection. A gas connection quote was not received prior to the completion of this study therefore an estimate figure based on similar projects has been used in the assessment.

A mains water supply and drainage will be required for energy centre.

7.2.8 Metering

All metering should be specified with suitable accuracy class in accordance with the Measurement Instrumentation Directive to satisfy the utility requirements for the purchase and sale of heat, gas, water, and electricity for the energy centre.

Heat

The energy centre will have at least three heat meters installed: one combined mine water heat pump heat meter, a combined gas boiler heat meter and a combined export heat meter. The ultrasonic flow sensors measure flow and return temperatures and flow rates and the multi-function meters will calculate the heat energy exported. The heat meters will provide output signals (via Mbus) for instantaneous measurements and cumulative measure of flow and energy. Data from all meters will be imported into the control system and used for control and monitoring of system performance.

Water

There will be water meters to determine the cumulative use by each of the system pressurisation units, water treatment plant and the overall incoming mains water to each of the energy centres. All data will be collected by the control system.

Electricity

Electricity meters will be fitted to measure the supply to the heat pumps and the import electricity from the grid.

7.3 Building Connections

All network connections are assumed to be indirect (where a heat exchanger separates the heat network hydraulically from the building space heating and hot water systems). The commercial connections will consist of a heat substation.

The HIU and substation packages will include:

- Supplier meter to meter all heat usage on the primary side of the connection.
- Two-port differential pressure control to control the supply flowrate and temperatures across the heat exchanger via two-port control methodology. Control valves can either be a single PICV or a DPCV with a separate two-port control valve.
- Plate heat exchanger (PHE) at which the district heat is transferred to the customer secondary side network. PHEs will be specified with a maximum 3°C temperature drop between primary and secondary side and a maximum 80kPa pressure drop on the secondary side of exchanger.
- Means of flow measurement and test points on both sides for commissioning purposes.
- Filtration to protect the plate heat exchangers and valves from fouling.
- Flushing, filling and draining details for chemical flushing of all pipework on the primary and secondary side.
- Pressure relief, control and instrumentation to allow the supplier control and monitor of the supply of heat.

Commercial Connection

The commercial connections will consist of a heat substation. The substation includes heat exchangers, control valves and heat metering and will be maintained by the network operator. The substation can include one or more plate heat exchangers (PHEs) (two shown in the example in [Figure 45\)](#page-73-0), depending on the size, turn-down and redundancy required for each building. Typically, two PHEs are installed in parallel, each installed at 60% of peak load, provide a full thermal range, and some redundancy to permit service and maintenance periods. Larger substations may include more than two PHEs. Only the key functional features are shown in the simplified schematic in [Figure 45.](#page-73-0)

Figure 45: Example of typical substation connection for commercial development

Residential Connection

The HIU includes a plate heat exchanger for the space heating, a plate heat exchanger for instantaneous domestic hot water, pressure independent/differential pressure control valves and a heat meter. The key functional features are shown in the simplified schematic i[n Figure 46.](#page-74-0)

HIUs are comparable in size to a domestic combination boiler and are usually wall hung. The hot water is best provided via an instantaneous PHE with a suitable means to ensure the network side of the plate is controlled (to ensure satisfactory hot water supply response to dwelling taps whilst minimising the supply pipework heat losses during standby periods). Space heating supply will be an in-direct connection (where a PHE is used to transfer supply heat into the secondary circuit).

The location of the HIU should be as close as possible to the main district heat network to minimise pipe lengths and network losses. Ideally the HIU will be accessed from outside the dwelling to enable access for maintenance.

The utilities required for the HIU are:

- 240 V spur connection
- 15 mm mains cold water service (MCWS) connection
- Suitable drain point

7.4 Heat Network

7.4.1 Futureproofing

The optimised network route has been designed to consider possible future connections with the main network leaving the energy centre allowing for sufficient over capacity. The connections to the clusters have been consider in section [5.3.](#page-45-0) For the TEM assessment no private housing has been considered to connect. However, the spine and branch connections to the connected clusters have been sized to allow full connection of private houses in these clusters to ensure that private dwellings could connect to the network if they choose. The PEX pipework that will be used in the housing clusters allows hot tapping to connect additional dwellings without disturbing network operations.

7.4.2 Operating Conditions

A detailed assessment of the proposed network has been undertaken and the proposed operating conditions reflect the optimal network efficiency. To effectively serve the existing connections and new build developments the heat network will operate with variable temperature conditions based on the ambient outside temperature to reduce heat losses as much as possible.

7.4.3 Optimised Route

The pipe routes have been designed to consider pipe length and barriers such as existing utilities, highways and construction limitations (see sectio[n 5\)](#page-42-0). The network has been designed with futureproofing to allow expansion of the scheme. Where social housing clusters have been connected to the network, the spine has been designed to allow connection of all private housing in that cluster.

7.4.4 Pipe Sizing and Insulation

The prioritised network route was imported into network modelling software to determine the characteristics and sizing for each part of the network with the aim of minimising pumping energy costs and heat losses in the network. The software allows different scenarios to be modelled and pipe characteristics, such as velocity, pressure loss and temperatures in the pipe are calculated to determine the optimum pipe size. Energy centre pumping requirements are also considered to ensure the optimum pipe size is selected. [Figure 47](#page-76-0) shows an example output displaying pipe velocity under diversified load conditions.

Figure 47: Pipe velocity under diversified load conditions

7.4.5 Network Costing

Factors considered when costing the network include dig conditions, percentage of straight or curved pipework, number of elbows, joints etc. Additional cost elements such as traffic management and avoiding utilities were added to sections of the network where appropriate.

Figure 48: Example of optimised network sizing

8 TECHNO-ECONOMIC MODELLING

A TEM has been constructed to assess the economics of the prioritised heat pump network option. The key assumptions for the TEM and key parameters are shown in Appendix 6: [Techno Economic Modelling](#page-125-0) – Key Parameters.

The sensitivity of all key assumptions and energy tariffs has been assessed, see section [10.1.](#page-87-0) The TEMs provided with this report allows key variables to be revised and the associated impact assessed.

8.1 Model Structure

[Figure 49](#page-78-0) shows an overview of the tabs included in the TEM. Tabs relevant to the standard user are shown in grey. These tabs include the key model inputs and variables and display the key results from the model. Tabs that involve technical inputs and calculations are shown in green. Inputs in these tabs have been input from the SEL technology sizing tool (see [Appendix 5:](#page-121-0) [Technology Sizing\)](#page-121-0) and are set for each phase. A user guide and full list of assumptions have also been included in the TEM.

Figure 49: TEM tab structure

8.2 Energy Tariffs

8.2.1 Energy Sales Tariffs

Energy sales tariffs used in economic assessments have been based on heat network energy tariffs used by clients from previous projects for commercial connections. These have been calculated based on the current cost of heat. Tariffs are made up of a variable tariff, daily standing charge and capacity charge. Energy sales tariffs have been set for each individual network connection based on the required connection capacity and annual heat demand and BEIS price projections have been used, as stated i[n Appendix 3: Key Parameters and Assumptions.](#page-114-0) These can be varied in the TEM.

8.2.2 Energy Centre Tariffs

Due to current energy crisis and uncertain energy prices gas and electricity purchase tariffs for the energy centre have been based on October 2022 commercial price cap energy tariffs. CCL has been included for all gas required for the peak and reserve

boilers and all electricity imported from the national grid. These proposed rates have been used (0.775 p/kWh for electricity and 0.672 p/kWh for natural gas).

8.3 Initial Capital and Replacement Costs

Technology replacement costs are modelled on an annualised basis and consider the capital costs, expected lifetime, fractional repairs and the length of the business term. Details of expected equipment lifetime and fractional repairs are shown in [Appendix 3: Key Parameters and Assumptions.](#page-114-0)

Capital costs for the scheme are based on a combination of previous project experience, quotations for recent similar works and soft market testing. Soft market testing has been conducted with potential suppliers of plant and equipment.

To develop an accurate estimate of the heat network costs, the proposed network has been broken down into constituent parts (i.e. straight pipe lengths, pipe bends, valves, valve chambers, welds, weld inspections, etc.) for each pipe section. These quantities have then been multiplied by the average rates taken from numerous quotations obtained for similar work. A complexity factor has been added to this to account for the areas of lower implementation or construction complexity and areas of higher complexity such as main roads, key intersections and areas of congested utilities. This value was then assessed against the price provided via specific soft market testing.

Estimated capital costs for key plant items (such as heat pumps, thermal storage tanks, etc.) have been obtained from the respective suppliers.

By using the above methodology, CAPEX estimates are within the tolerance stated in the project requirements and ITT and contingency has been applied to each element of capital expenditure as appropriate. A breakdown of capital costs and contingency values for each phase are shown in Appendix 6: [Techno Economic Modelling](#page-125-0) – Key Parameters.

8.3.1 Connections Cost and Connections Charges

It has been assumed the network operator covers costs of all connections due to the high proportion of council owned sites. A connection charge could be charged to private connections based on avoided costs of installing low carbon heating which would improve network economics. Connection charges for all planned developments have been included in the base case assessment as the avoided costs of installing individual ASHPs at £8,125 per dwelling.

8.4 BEIS Energy Price Projections

To assess the impact of expected future price changes on the financial outputs, the BEIS central scenario price projections for natural gas and electricity have been used (last updated June 2021). The projected changes in prices for electricity and natural gas for residential, services and industrial is illustrated in [Figure 50.](#page-80-0) The projected price variations have been applied to the energy tariffs calculated as discussed in section [8.2.](#page-78-1)

Figure 50: BEIS price projections – central scenario, updated June 2021

The above projections indicate that while both gas and electricity prices are predicted to increase in the short and medium term, in the long term, electricity prices are expected to show a decreasing trend, while gas prices continue to increase. This will result in improved viability of heat from heat pumps. The BEIS low and high scenarios, as well as a fixed indexation rate has also been assessed for the network option and their effect is shown in section [10.1.](#page-87-0)

8.5 Network Summary

A summary of the network is shown in [Table 23.](#page-80-1) Figures shown give later phases as additional to the previous phase, the total column shows figures for the fully built out network.

| | Phase 1 | Phase 2 | Phase 3 | Total |
|--|--------------|--------------|--------------|--------------|
| Network heat demand | 10,690 MWh | 3,005 MWh | 4,884 MWh | 18,579 MWh |
| Network spine trench length | 2,572 m | 1,206 m | $1,103 \; m$ | 4,880 m |
| Feed and cluster trench length | $6,252 \; m$ | $3,149 \; m$ | 10,383 m | 19,784 m |
| Network spine linear heat density | 4.2 MWh/m | 2.5 MWh/m | 4.4 MWh/m | 3.8 MWh/m |
| Network losses | 1,113 MWh | 450 MWh | 1,212 MWh | 2,793 MWh |
| Heat pump capacity | 2.51 MW | 0.74MW | 0.56 MW | 3.81 MW |
| Heat supplied by heat pump | 11,707 MWh | 3,433 MWh | 5,189 MWh | 20,329 MWh |
| Heat supplied by peak and reserve gas boilers | 0.308 MWh | 0.128 MWh | 0.541 MWh | 0.977 MWh |
| % low carbon / renewable heat | 97% | 97% | 95% | 95% |
| Estimated phase start year | 2024 | 2026 | 2028 | |

Table 23: Network summary

8.6 Economic Assessment

The 25 year, 30 year and 40 year economic assessments for each phase of the network are shown in [Table 24.](#page-81-0) Detailed breakdown of capital costs and contingency are shown in Appendix 6: [Techno Economic Modelling](#page-125-0) – Key Parameters.

Table 24: Economic assessment

The capital costs, operational expenditure, revenue, and cumulative cash flow for the full network is shown in [Figure 51](#page-81-1) for 40 years.

Figure 51: Heat network - cumulative cash flow - 40 years

8.7 Green Network Fund

BEIS provides capital support for heat network developments seeing them as a key part of delivering the UK's legally binding commitment to achieve net zero by 2050. As such they have made capital support available to projects via the Green Heat Network Fund (GHNF) which is launched in April 2022.

GHNF is a £288m fund available to support heat network project with capital grants available to up to but not including 50% of the project capex.

[Table 25](#page-82-0) shows GHNF criteria and preferred option parameters.

Table 25: Green Heat Network Fund core metrics

The GHNF grant is required to be spent by end of 2025 if a scheme is awarded. Therefore, only Phase 1 is likely to be spent within this period. If the maximum grant funding (49%) is achieved for Phase 1 then the project economics are given i[n Table](#page-83-0) 26.

Table 26: Economics assessment with 49% GHNF in Phase 1

The capital costs, operational expenditure, revenue, and cumulative cash flow for the full network with GHNF funding in Phase 1 is shown i[n Figure 52](#page-83-1) or 40 years.

Figure 52: Heat network - cumulative cash flow with GHNF in Phase 1 - 40 years

9 ENVIROMENTAL BENEFITS AND IMPACTS

The following section describes the benefits and impacts associated with the recommended network options. The CO2e emissions have been assessed annually for each phase for 40 years. This has been compared to the business as usual (BAU) emissions and overall CO2e savings calculated.

9.1 CO2e emission assessment

The CO2e emissions have been assessed annually for each network option for 25, 30 and 40 years. This has been compared to the business as usual (BAU) emissions and overall $CO₂e$ savings calculated.

CO2e intensity projections for grid electricity and natural gas are shown i[n Figure 53.](#page-84-0) The CO₂e emissions for the electricity grid are expected to reduce over time due to the increase in wind, solar and nuclear power and the closure of coal power stations.

Two CO2e projections for grid electricity have been considered:

- BEIS long run marginal figure (commercial)
- BEIS long run marginal figures (residential)

The BEIS marginal emissions factors consider the marginal plant for electricity generation. The projections are based on assumptions of future economic growth, fossil fuel prices, electricity generation costs, UK population and other key variables which are regularly updated. They also give an indication of the impact of the uncertainty around some of these input assumptions. Each set of projections takes account of climate change policies where funding has been agreed and where decisions on policy design are sufficiently advanced to allow robust estimates of policy impacts to be made.

These figures have been used for all electricity imported from the grid (i.e., for heat pump and energy centre electricity demand).

Figure 53: CO2e emissions projections, updated June 2021

9.1.1 Network emission

Individual gas boilers have been assessed as the carbon emissions base case BAU for the network. BAU CO₂e emissions, network $CO₂e$ emissions and $CO₂e$ savings for the network are shown in [Figure 54](#page-85-0) and [Table 27.](#page-85-1) The yellow line shows the difference between CO2e emissions in the BAU emissions and the network emissions. The BAU emissions remain constant due to the constant natural gas emissions factor used in assessments and only increases with the increase in heat demand with each network phase. The network emissions reduce marginally over time as the grid decarbonises. Carbon savings compared with individual ASHP would be negative as network distribution losses are avoided.

Figure 54: Network CO₂e emissions and savings – 40 years

Table 27: Network CO₂e emissions and savings

The CO₂e intensity of heat delivered in the first year of network operation (91 gCO₂e/kWh) is significantly lower than the SBEM/SAP (2012) figure for notional building connected to a district heat network of 190 g/CO2e/kWh, proposed 350 gCO2e /kWh threshold for existing network in the Part L 2022 uplift and GHNF criteria of 100 gCO2e/kWh.

9.2 Air Quality

Gas boilers have been included in the base case, they should be compliant with the Medium Combustion Plant Directive. Gas boilers will be low NOx versions and will run only at peak heat demands and when the heat pumps are not operating. The low carbon technology has been sized to meet >90 % of the network heat demand in wherever possible.

If electric peak and reserve boilers are installed, they will decrease the economic viability of the network due to the increased cost of electricity versus gas and the increased fixed charge based on required capacity (particularly in the short term) and significantly increase risk associated with the resilience and reliability of the centralised heat pumps (if the heat pumps are unavailable for significant periods, the operation electric peak and reserve boilers may be an unacceptable risk for O&M contractors obligated to deliver heat at a specific price).

Dispersion modelling should be conducted at detailed project development (DPD) stage, if a district heating project is progressed with gas boilers, to ensure that any impact is within regulatory limits and meets local air quality objectives (and this information will be fed back into the flue design process). Air dispersion analysis simulates the exhaust gases for each hour and models the dispersion of gases and, where appropriate, particulate emissions (although these are considered negligible for natural gas fuelled plant) over a wide geographical area. The output of the analysis provides concentrations levels of particulates and NOx at specified locations.

9.3 Social IRR and NPV

The environmental benefits to the scheme are determined by monetising the $CO₂e$ savings and the improvements in air quality against the use of individual gas boilers. The economic value of the carbon and air quality improvements are included in the project cashflow to generate a social IRR and NPV, shown in [Table 28.](#page-86-0) The social IRR helps to identify the wider benefits of the scheme for the community and is a vital consideration for local authorities.

Table 28: Social IRR and NPV

10 SENSIVITY ANALYSIS, RISK AND ISSUES

10.1 Sensitivity Analysis

Sensitivity analysis has been undertaken for the prioritised network based on the key network risks, parameters, and variables. The base case 40-year IRRs are shown in grey cells in the tables.

Key risks for the network include:

- Capital costs
- Grant funding
- Network heat demand and key sites not connecting
- Energy tariffs including heat sales tariffs, energy centre fuel purchase tariffs and indexation of energy tariffs
- Heat pump SPF

10.1.1 Capital Cost

The effect of a variance in capital costs is shown in [Figure 55](#page-87-1) for each network phase. A decrease in capital costs of approximately 9% would be required for Phase 1 to achieve a positive 40-year IRR.

A cost of £2,000 per m² (£2,300 with contingency) has been used for the energy centre building and assumes an industrial unit standard building specification. Should the Phase 1 energy centre be designed to a higher specification with additional architectural design, the costs could increase as high as £4,000 per m² (not including contingency). This would increase the overall CAPEX by 10.2% and result in a 40-year IRR of 0.9%.

[Figure 55](#page-87-1) shows the 40-year IRR for each network phase

Figure 55: Variance in capital costs

Generation and Supply CAPEX

[Table 29](#page-88-0) shows the effect of an increase of generation and supply CAPEX, this would result in a significant impact on the 40-year IRR.

Table 29: Effect of an increase in generation and supply technology CAPEX on Phase 1

Network CAPEX

[Table 30](#page-88-1) shows the effect of an increase network CAPEX, this would result in a significant impact on the 40-year IRR.

Table 30: Effect of an increase in network CAPEX

10.1.2 Green Heat Network Fund

[Figure 56](#page-88-2) shows that the maximum available grant (49%) achieves a Phase 1 40-year IRR of 5.9%. This is with grant funding only applied to the capital spend in Phase 1. It assumes the other phases do not receive additional grant funding.

Figure 56: Impact of grant funding on 40-year IRR

10.1.3 Heat Demand

[Figure 57](#page-89-0) shows the effect of a variance in the total network heat demand for each phase, with all other parameters remaining constant. A reduction in heat demand results in a detrimental reduction in the 40-year IRR, this is due reduction in kWh sold but capital cost remaining constant. An increase in heat demand is shown to have a positive impact on the IRR for all phases. This is due to the heat pump increasing heat output in response to the increased demand and keeping the percentage of heat

from the heat pump at a similar level. The cost of heat from the heat pump is cheaper than the gas boilers at the assumed energy input tariffs. It does not consider the installation of additional or larger capacity heat pumps.

Variance in heat demand

Figure 57: Variance in heat demand

[Table 31](#page-89-1) shows the impact of the key buildings not connecting to heat network. If these buildings do not connect, then the network may not be viable. There is a large social housing demand that will negatively affect the network if they are not connected.

Not connecting planned development has a negative effect on the Phase 3 IRR, mainly due to the assumed heat connection fee being lost. Therefore, if the developer is not engaged at an early stage, then it may not be economically viable to proceed with Phase 3 and therefore a large section of social housing will not connect to the network and alternative low carbon heating arrangements for these dwellings will need to be found.

Table 31: Impact of buildings not connecting to the network

10.1.4 Energy Tariffs

Energy Centre Gas Tariffs

[Figure 58](#page-90-0) shows the effect of a variance in gas purchase price for the energy centre. For the base case assessment, a gas tariff of 7.5 p/kWh has been used. It can be seen that energy centre gas tariff has little impact on the 40-year IRR as the scheme uses gas only to supply peak and reserve, therefore it has a very low gas demand. (> 95% of the heat demand is met by low carbon technology).

Figure 58: Variance in gas purchase price, p/kWh

Energy Centre Electricity Tariffs

[Figure 59](#page-90-1) shows the effect of a variance in electricity purchase tariff for the energy centre. For the base case assessment, 21 p/kWh for day and night electricity tariff has been used.

This has a significant effect on the 40-year IRR for all network phases as all the energy centre electricity demand is met by import from the grid and makes up the highest operational expenditure for the network.

Heat Sales

[Figure 60](#page-91-0) shows the effect of a variance in heat sales tariff. It has been assumed as a base case that the variable element of the heat sales tariff will vary in line with the cost of electricity (based on the BEIS central scenario price projections for electricity). Heat sales tariffs have been calculated as a 3% saving on an ASHP counterfactual.

Variance in heat sales tariffs

Figure 60: Variance in heat sales tariffs

Energy centre gas tariffs and heat sales

[Figure 61](#page-91-1) shows the effect of a variance in heat sales tariff and gas purchase price. It has been assumed as a base case that the variable element of the heat sales tariff will vary in line with the cost of gas (based on the BEIS central scenario price projections for natural gas). As only about 3% of the total demand is met by gas, its impact on the 40-year IRR is minimal. As a result, an increase in the heat sales tariff and the price of gas purchased results in a major increase in the IRR due to the increased heat sales and minimal impact of the gas price.

Variance in gas purchase tariffs and heat sales, p/kWh

Figure 61: Variance in gas purchase tariffs and heat sales

Energy centre electricity tariffs and heat sales

[Figure 62](#page-92-0) shows the effect of a variance in heat sales tariff and electricity purchase price. It has been assumed as a base case that the variable element of the heat sales tariff will vary in line with the cost of electricity (based on the BEIS central scenario price projections for electricity). An increase in heat sales and electricity purchase price has a smaller impact on the 40-year IRR than an increase in heat sales and gas price. Due to the fact that the price of electricity is a key variable in determining the

viability of the heat network. Therefore, the advantages of the increased heat sale tariff will be diminished when electricity purchase price increases.

Variance in electricity purchase tariffs and heat sales, p/kWh

Energy Price Indexing

The effect of price indexing on all energy tariffs is shown in [Table 32.](#page-92-1) If tariffs are indexed at a fixed rate, this reduces the 40-year IRR for all phases.

Table 32: Effect indexing on all energy tariffs

[Table 33](#page-92-2) shows the effect of assuming variable heat sales tariffs only, and fixed and variable tariffs. In the base case, it has been assumed that the heat sales tariff would include a fixed and variable element with the variable tariff fluctuating in line with the BEIS natural gas price projections and the fixed tariff remaining constant. It is recommended that there is a fixed and variable element to the heat sales tariff. Table below shows the importance of the split between fixed and variable tariffs as with variable heat sales tariffs only has a negative effect on the 40- year IRR.

Table 33: Effect of variable and fixed heat sales tariffs

Figure 62: Variance in electricity purchase tariffs and heat sales

10.1.5 Availability of Heat

In the base case it has been assumed that the heat pumps would operate for 50 weeks of the year. If this was reduced it could have a negative effect on the IRR, carbon intensity and network economics, as shown in [Figure 63.](#page-93-0)

Variance in weeks of availablilty per year of low carbon technology

10.1.6 Heat Pump SPFH2

[Figure 64](#page-93-1) shows the effect of variance in the SPF_{H2} of the heat pumps. SPF_{H2} includes electrical input measurements of heat pump and abstraction pumps. If the electricity requirements for abstraction pumps increase, the project IRR will decrease.

Variance in SPF_{H2}

Figure 64: Variance in SPF_{H2}

10.2 Sensitivity Summary

Key sensitivity parameters for the prioritised network areas include:

- Capital costs
- Network heat demand and key sites not connecting
- Energy tariffs including heat sales tariffs, energy centre fuel purchase tariffs and indexation of energy tariffs
- Grant funding

10.3 Risk and Issues

The main risks and constraints for the implementation of the proposed district heating network options have been considered and assessed. [Table 35](#page-95-0) outlines potential risks and issues that apply to all networks including both current risk and re-scored values.

Risk ratings are the product of impact and likelihood. The impact measures how much of an affect the risk being realised would have, and the likelihood is a measure of how probable the risk realisation is. The score associated with current risk is the level of risk present if no further action is taken, and re-scored risk levels are a measure of the risk present once the mitigating measures have been carried out.

A key showing the level of risk is shown i[n Table 34.](#page-94-0)

Table 34: Risk level key

11GOVERNANCE, COMMERCIAL AND PLANNING POLICY CONSIDERATIONS

This section sets out the key considerations for commercial and governance structures to progress a district heat network project in the Killingworth area. North Tyneside Council have several options to consider and these include doing nothing by allowing the scheme to be private sector led, or playing a leading, supporting and facilitating role for any network developments.

NTC-led scheme

If the economics of the scheme do not attract private investment and the project is still to be carried forward, then NTC could play a more active role in the network development. This could either be via direct operation of the network or by setting up a Special Purpose Vehicle (SPV) to own and operate the network. An NTC-led SPV would allow NTC to retain control and ensure project priorities are implemented and potentially provide access to grant funding while allowing flexibility. However, there may be some potential for partnering with private sector stakeholders. Key roles including design, build, operate and maintain will be outsourced.

If the scheme is to be NTC-led then it is likely that a Special Purpose Vehicle (SPV) will need to be set up to operate as an Energy Services Company (ESCo), owning and operating the network. The ESCo will need to contract with specialist companies for the design, build, operation and maintenance of the schemes and, potentially, to sell heat to customers. The ESCo would then be responsible for volume and price risk, however these can be mitigated through diverse customer bases, fixed charge elements, termination notices and indexing of heat sale prices.

BEIS has established a dynamic purchasing system (DPS) for heat networks - the BEIS Heat Investment Vehicle (BHIVE). It will allow public sector heat network owners and developers to procure funding and funding-related services for their heat network projects from a range of potential funding providers. All public sector applicants seeking provisional GHNF awards must notify the BEIS Heat Investment Vehicle (BHIVE) to consider suitability of the project for third party funding and this should be the preferred method for seeking third party finance for such projects. Engagement with BHIVE is required to understand the potential opportunities for third party funding.

[BEIS Heat Investment Vehicle](https://tp-heatnetworks.org/bhive/) – GHNF (tp-heatnetworks.org)

Private sector-led scheme

If the scheme is to be private sector-led, then grant funding is likely to be required and project risks will need to be minimised to allow a private company to take a long-term view on investing in the network. Risk to the private sector company would need to be reduced by:

- Ensuring that every new development connects to a network
- Ensuring all large public sector heat loads connect
- The provision of NTC-owned land for network pipes and generation assets
- Where risk cannot be fully accepted by the private sector party, pre-agreed risk sharing (e.g. demand / revenue guarantees)

As heat networks are becoming a key part of the governments climate change policy more private sector investment is becoming available, and lower rates of return may be acceptable for private sector companies that can take a long term view on the investment.

11.1 Planning Policy

Planning policy can be used to promote and facilitate the development of district heat networks and the NTC planning team has an important role to play in developing and supporting guidance and working with developers. NTC and its planners are critical to the effective development of heat networks in that they:

• Develop the planning policy that sets out requirements for developers to comply with CIBSE/ADE CP1 standards

- Influence financial mechanisms / developer contributions that can support the strategic development of heat networks
- Promote the benefits of the project to developers
- Set out heat priority areas within development plans
- Safeguard network routes and energy centre sites in development plans
- Identify carbon reduction targets for strategic sites in development plans
- Review energy statements and set viability requirements for district heating connection

The findings and recommendations in this study should inform policy, guidance, and developer engagement.

11.1.1 National Policy

The key national policy objectives for district heat networks are:

- National Planning Policy Framework (2012) promotes sustainable development and encourages local authorities to establish low carbon energy generation schemes
- The future of heating: Meeting the challenge (2013) heat networks are included as one of five options for building heat infrastructure
- Clean Growth Strategy (2017) promotes the building and extension of heat networks across the country
- National Policy Statement for Renewable Energy Infrastructure EN-3 promotes development of new energy infrastructure to deliver a secure, diverse, and affordable energy supply
- UK's 2050 net zero target (2019) to bring all greenhouse gas emissions to net zero by 2050
- National Planning Policy Framework update (2019) states that developments should identify opportunities to draw their energy supply from decentralised, renewable, or low carbon energy supply systems
- New Part L (2021) building regulations have been implemented in June 2022 and aims to reduce CO2e emissions of dwellings by 31% compared with current levels – with gas boiler heating:
	- o Significant improvement in building fabric
	- o 40% ground floor area in solar PV
	- o Waste water heat recovery
	- o Maximum supply temperatures of 55°C to allow for future low carbon heating
- Future Homes Standard (expected in 2025) aims to reduce CO2e emissions of dwellings by 75-80% compared with current levels
	- o Requires low carbon heating (no gas boilers)
	- o Slight improvement in building fabric (compared with 2021)
- Heat and Building Strategy (2021) sets out the government ambition to phase out the sale of gas boilers by 2035
- Consultation: Proposals for heat network zoning (2021) proposal for central government, local government, industry and local stakeholders to designate areas within which heat networks are the lowest cost, low carbon solution for decarbonising heating

11.1.2 Planning Recommendations

NTC should undertake further corporate actions to promote and enable schemes including:

- Provision of council-owned land for energy centres, substations and pipe routes
- Engagement and support with planning consents and highways activities for networks
- Providing resource and financial assistance to deliver feasibility and design work for the network
- Use the evidence provided in this report to inform planning requirements and engagement activities for specific developments
- Provide resource and financial assistance to deliver project development and design work for the network
- Produce a developer's pack to inform developers of the requirements for their developments to develop/connect to district heating schemes (to include short, medium and long term considerations e.g. the timing of the proposed project)

12CONCLUSION

The conclusions for the Killingworth Feasibility Update Study are outlined discussed below.

Energy Demand Assessment

The total estimated heat demand for the Killingworth area is 70.4 GWh. Private housing accounts for 61% of this heat demand. However, for the purposes of this study private housing has been discounted as a connection to a heat network as it was assumed that challenges in connecting and engaging individual private dwellings at this stage are too great.

After excluding private dwellings from the network demands, council owned and operated buildings (including social housing) account for 49% of the demand, private sector 35% and planned developments account for 16% of the estimated 27.4 GWh of heat demand. Key heat demands include NTC Killingworth Site, Matalan/Home Bargains and Morrisons in the town centre shopping area.

Actual half hourly gas data was available for all large council sites. No data was received for private commercial connections. Where actual data was not available the energy demand assessment has been performed using high level building information and use type and should be reviewed when such information becomes available.

Energy Supply Assessment

Heat pumps, waste heat, biomass and gas CHP technologies were assessed as options to supply potential heat networks. The key potential source of renewable heat has been identified as mine water for water source heat pumps (WSHPs).

In discussion with North Tyneside Council officers, the preferred energy centre location is the Killingworth Depot site. This is a council owned site adjacent to the Killingworth Site. The site is also ideally located as it sits directly above four potential mine seams.

Network Assessment

The network was assessed over three phases. Phase 1 connections have been assessed as low risk connections, they include existing council buildings, social housing clusters located close to the main network spine and large commercial connections in Killingworth town centre. Phase 2 extends to connect larger connections in the northern industrial site as well as Burradon School and the adjacent social housing cluster. Phase 3 includes long term planned housing development at Killingworth Lane and the high density social housing cluster near to this development.

The DH network will be developed over three phases (see below):

Killingworth Depot Energy Centre Concept Design

Technology sizing scenarios have been assessed to determine the optimal heat pump and thermal store for each network phase. The optimised solution includes a 2.5 MW mine water heat pump installed at Killingworth Depot in Phase 1, with an additional 0.74 MW mine water heat pump in Phase 2 and 0.56 MW mine water heat pump in Phase 3. 200,000 litres of thermal storage will be installed for Phase 1. The fully built out energy centre requires a land area of approximately 693m².

The scheme will also require peak and reserve gas boilers for times of peak demand (e.g. during coldest weather) or when the renewable or low carbon plant is not operational. The peak and reserve boilers would be located within the energy centre.

Scheme CAPEX

Capital costs for the scheme are based on a combination of previous project experience, quotations for recent similar works and soft market testing. Soft market testing has been conducted with potential suppliers of plant and equipment.

A summary of the scheme CAPEX is shown in table below.

Economics

The 25-year, 30-year and 40-year economic assessments for each phase of the network are shown in table below.

The economics of the heat network are marginal and grant funding is likely to be required. This is available through the Green Heat Network Fund for new and existing district heat networks designed to increase the utilisation of low-carbon heat in district heat networks in the UK. There is also potential for regulations and taxation to further disincentivise or ban the use of fossil fuel heating systems.

Key Sensitivities and Risks

Key sensitivity parameters for the prioritised network areas include:

- Capital costs
- Network heat demand and key sites not connecting
- Energy tariffs including heat sales tariffs, energy centre fuel purchase tariffs and indexation of energy tariffs
- Grant funding

Key risks that should be addressed by NTC whenever possible are:

- Securing energy centre site,
- Developing planning policy for new developments requiring to investigate low carbon heating solutions
- Procure Stage 2 Coal Authority report to confirm mine water available flowrates and therefore heat capacities
- Engagement with Northumberland Estates about development at Land Off Killingworth Lane,
- Engagement with GHNF team to fully understand requirements to ensure a robust grant funding bid is submitted

The network is reliant on suitable energy centre locations being secured. The Killingworth Depot energy centre site was highlighted as a priority site for an energy centre by North Tyneside Council officers. Following consultation from the Coal Authority the energy centre site is likely to be a suitable location to abstract and re-inject mine water. However, the available flow rate and temperatures from the mines requires further investigation.

13NEXT STEPS

The following next steps and recommendations should be considered to progress the scheme:

APPENDIX 1: ENERGY DEMAND ASSESSMENT

Table 36: Key energy loads

APPENDIX 2: HEAT DEMAND MODELLING METHODOLOGY

Using data provided by the council, we were able to group every residential dwelling in the assessment area into both an age band, and one of five property types: Detached, Semi–detached, End–terrace, Mid–terrace, and Flats. By taking multiple measurements from 3D models, available on Google Earth, we were able to obtain an 'average' Killingworth house for each property type. Dwellings were assigned U–values based on property age which, in combination with average building layouts, allowed us to produce heat demand models for each type of property, and for each age band. U–values were taken from 'The Government's Standard Assessment Procedure (SAP) for Energy Rating of Dwellings' 2012, as show i[n Table 37.](#page-112-0)

Table 37: U–values used in heat demand assessment

[Table 38](#page-112-1) shows the heat demand benchmark figures (kWh/m²) calculated under consideration of factors such as building layouts, occupancy assumptions, estimated solar gains, and hot water usage, for each type of residential dwelling assessed.

Table 38: Heat demand benchmarks (kWh/m²)

A weighted average heat demand benchmark (kWh/m²) was calculated for each cluster, this was calculated as follows:

$\Sigma\,(\frac{No.\,of\,properties\,of\,specific\,type\,\&\,age}{Total\,no.\,of\,properties\,in\,cluster})\times (kWh/m^2\,for\,property\,of\,specific\,type\,\&\,age)$

Killingworth area has been split into clusters and differentiated by housing type: social or private. To determine heat demand of each cluster heat demand benchmark developed from heat demand models and floor areas provided by council were used.

Table 39: Heat demand modelling results

APPENDIX 3: KEY PARAMETERS AND ASSUMPTIONS

Energy Tariffs

Energy sales tariffs used in economic assessments have been based on heat network energy tariffs used by clients from previous projects for commercial connections and average domestic tariffs for the area for residential connections. These have been calculated based on the current cost of heat. Tariffs are made up of a variable tariff, daily standing charge and capacity charge. Energy sales tariffs have been set for each individual network connection based on the required connection capacity and annual heat demand and BEIS price projections have been used. These can be varied in the TEM.

An example calculation for the heat sales tariffs used in assessments for commercial sites is shown in [Table 40.](#page-114-0)

Table 40: Example commercial heat sales tariffs calculation with ASHP counterfactual

Table 41: Current residential tariffs

Final heat sales tariffs derived based on the counterfactual options, ASHP for commercial buildings and planned development and gas boilers for social housing clusters are shown in [Table 42](#page-114-1) an[d Table 43.](#page-115-0)

Table 42: Heat sales tariffs calculated from cost of heat using low carbon counterfactual (ASHPs)

Table 43: Heat sales tariffs calculated from cost of heat using gas boiler counterfactual

Energy Centre Tariffs

Gas and electricity purchase tariffs for the energy centre have been based on current energy tariffs for existing energy centres, identified in previous projects. CCL has been included for all gas (if selected) required for the peak and reserve boilers and all electricity imported from the national grid. These proposed rates have been used (0.775 p/kWh for electricity and 0.672 p/kWh for natural gas).

Key Technology Parameters

Key technology parameters for the network are shown i[n Table 44.](#page-116-0) Heat pumps COPs and capacities come from manufacturer performance curves based on the Solid Energy LW252, LW172, LW170 heat pump models. Mine water temperature available was assumed to be 12 °C. The yield of each borehole was assumed to be 60 l/s.

Table 44: Technical inputs

Technology replacement costs have been calculated on an annualised basis and take into account the expected lifetime of the technology, fractional repairs and the length of the business term. Plant / equipment lifetimes are shown in [Table 45.](#page-116-1)

Table 45: Plant and equipment lifetime

Table 46: Energy centre building costs

BEIS Energy Price Projections

To assess the impact of expected future price changes on the financial outputs, the BEIS central scenario price projections for natural gas and electricity have been used (last updated October 2020). The projected changes in prices for electricity and natural gas for residential, services and industrial is illustrated in [Figure 65.](#page-117-0) The projected price variations have been applied to the energy tariffs calculated as discussed in section [10.1](#page-87-0) above.

Figure 65: BEIS price projections, updated June 2021

The above projections indicate that while both gas and electricity prices are predicted to increase in the short and medium term, in the long term, electricity prices are expected to show a decreasing trend, while gas prices continue to increase. This will result in improved viability of heat from heat pumps. The BEIS low and high scenarios, as well as a fixed indexation rate has also been assessed for the network option.

The BEIS fossil fuel price projections (central scenario) are shown i[n Table 47.](#page-117-1)

| | Sector | /Units | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | .2026 | -2027 | 2028 | 2029 | 2030 | 2031 | 2032 | 2033 | 2034 | -2035 |
|-------------------------|-------------------|--------|------|------|------|------|------|------|-------|-------|------|------|------|------|------|------|------|-------|
| Electricity | Industrial | p/kWh | 12.4 | 12.9 | 13.0 | 12.7 | 12.7 | 12.8 | 12.9 | 12.8 | 12.5 | 12.3 | 12.4 | 12.2 | 12.0 | 11.8 | 11.6 | 11.5 |
| | Residential p/kWh | | 19.2 | 21.1 | 21.5 | 21.4 | 21.1 | 21.3 | 21.5 | 21.1 | 21.0 | 20.9 | 21.3 | 21.2 | 20.7 | 20.2 | 19.9 | 19.6 |
| | Services | p/kWh | 14.5 | 15.0 | 15.2 | 14.8 | 14.9 | 15.0 | 15.0 | 14.9 | 14.5 | 14.4 | 14.6 | 14.7 | 14.5 | 14.1 | 13.8 | 13.7 |
| gas Iral ក្ខ ខ | Industrial | p/kWh | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.7 | 2.8 | 2.8 | 2.9 | 2.9 | 3.0 | 3.0 | 3.1 | 3.1 | 3.1 |
| | Residential p/kWh | | 4.0 | 4.3 | 4.5 | 4.6 | 4.6 | 4.6 | 4.7 | 4.7 | 4.7 | 4.7 | 4.8 | 4.8 | 4.8 | 4.8 | 4.9 | 4.9 |
| | Services | p/kWh | 2.9 | 3.0 | 3.1 | 3.2 | 3.4 | 3.5 | 3.6 | 3.7 | 3.7 | 3.8 | 3.8 | 3.8 | 3.9 | 3.9 | 4.0 | 4.0 |

Table 47: BEIS fossil fuel price projections

CO2e Emissions Factors

The electricity grid CO2e emissions figures used in assessments are shown i[n Table 48.](#page-118-0)

Table 48: Electricity grid CO₂e emissions

Table 49: Natural gas CO₂e emissions

APPENDIX 4: NETWORK ASSESSMENT

The pipe routes have been designed to consider pipe length and barriers such as highways and construction limitations.

Pipe lengths, CAPEX and layouts are based on high level information provided and installing pipes in a coordinated manner and connecting houses in line with best practice. The dwellings on the right i[n Figure 66](#page-119-0) an[d Figure 67](#page-119-1) reflect the assumptions used and show shared feed pipes from the road to the front of the dwelling and heat interface units (HIUs) located at the nearest point to the network branches respectively. If this is not achieved, then additional network length will be required as shown in the dwellings on the left in [Figure 66](#page-119-0) and [Figure 67,](#page-119-1) and CAPEX and network heat losses will increase, which will significantly impact the scheme economics.

Figure 66: Shared feed pipes to terraced and semi-detached dwellings

Figure 67: Heat network connection and HIU location

The heat network has been assumed to be a pre-insulated ridged steel pipe system for larger pipe diameters and where possible flexible pre-insulated polymer pipe for smaller diameters. The pre-insulated pipe will either be installed as single pipe (with a separate pipe for the flow and the return) or twin pipe where both the flow and return pipe are housed within the same casing, se[e Figure 68.](#page-120-0)

Figure 68: Pipes in trench

Insulation will be CFC free rigid polyurethane foam homogenously filling the space between the service pipe and casing over the total length and in compliance with standard EN 253. The high density polyethylene (HDPE) pipe casing and all fittings and joints will be manufactured in compliance with EN 253 standards. The heat losses and size of trenches for the spine network have been based on a series two insulation thickness of polyurethane foam with diffusion barrier.

Pipework will include a pipe surveillance system in full compliance with BC EN 14419, suitable for both raising alarm of a fault and detecting the location of a fault within all routes of the network. The alarm system will allow provision of outputs to the energy centre control system.

Figure 69: Multi-utilities trench

When multiple utilities are present in a trench it is important to ensure that they are positioned a safe/workable distance from each other. The NJUG Guidance for Buried Utilities outlines how this can be achieved. [Figure 69](#page-120-1) shows an example of a multiutility trench.

APPENDIX 5: TECHNOLOGY SIZING

Energy generation technologies are assessed using in house software that has been developed to allow detailed sizing of plant and thermal storage, modelling of operating parameters and conditions, financial assessment, and sensitivity analysis. The software utilises hourly network demands for each day of the year and considers hourly energy outputs from low carbon technologies, thermal storage and peak and reserve plant considering modulation limits, efficiencies and plant down time for maintenance. A range of plant and thermal store sizes and number of units are assessed and optimised to ensure key operating and financial/investment criteria are met.

The tools consider:

- Heat and electricity demand that can be served by the plant (including private wire options)
- Thermal storage used to supply heat loads below modulation limits or peaks above plant capacity and minimise plant firing e.g. for heat pump, store size will be modelled, optimised and cost/benefit analysis conducted to consider the optimum operating strategy for heat generation
- Supply strategy consideration of issues such as varying seasonal or diurnal operation, continuous operation, modulated or full output, primary energy source or base load only and peak and reserve plant requirement
- Peak and reserve boiler sizing according to the diversified peak demand of the various network phases, predicted operating requirements and redundancy
- Peak supply and minimum load this will consider plant modulation limits and the number of units
- Carbon savings these will be calculated against the 'business as usual' case and include annual and lifetime savings based on the most up to date BEIS carbon emissions projections

Where heat pumps have been included, these have been sized based on network heat demand and have been maximised to provide the greatest economic and CO2e savings for the network option and to provide the optimum balance between heat generation capacity, capital cost, maintenance costs and physical size.

The heat pumps and thermal stores have been sized with consideration of the hourly annual network heat demand. Peak and reserve boilers will meet any remaining demand. Technology sizing is based on an iterative process within the technical model to identify the optimal balance of the priorities.

[Figure 70](#page-122-0) shows an output from our technology sizing tool for the full network served by 3.81 MW heat pump. The load duration curve shows the heat demand for every hour of a year, ordered from highest to lowest. The black line shows the total low carbon and renewable capacity installed in the energy centre. The heat demand above the black line is met by thermal storage and peak and reserve boilers.

Figure 70: Load duration curve for example network

[Figure 71](#page-123-0) and [Figure 72](#page-123-1) show the proportion of the heat demand supplied by the heat pump, charge and depletion of the thermal store and heat demand supplied by peak and reserve boilers for fully built network for 1st and 2nd January and 1st and 2nd August respectively. The heat pump and thermal stores meet the majority of the baseload heat demand with a small proportion of the demand met by peak and reserve boilers. Where the thermal store charge and depletion is greater than the total heat demand shown in [Figure 71](#page-123-0) and [Figure 72,](#page-123-1) the thermal store is being charged. Where the thermal store charge & depletion is below the total heat demand, the thermal stores are being depleted.

Figure 72: Heat generation 1st and 2nd August

Thermal stores have been sized based on hourly network heat demand, heat pump capacities, modulation limits and capital costs. [Figure 73](#page-124-0) shows the hourly operation of the heat pump for the example network with and without a thermal store. The thermal store provides significant benefits at times of peak network demand and when heat generation is restricted by modulation limits.

Figure 73: Load duration curve and thermal store usage

APPENDIX 6: TECHNO ECONOMIC MODELLING – KEY PARAMETERS

Initial Capital and Replacement Costs

Technology replacement costs are modelled on an annualised basis and consider the capital costs, expected lifetime, fractional repairs and the length of the business term. Details of expected equipment lifetime and fractional repairs are shown in the section "Key Technology Parameters"

Capital costs for the scheme are based on a combination of previous project experience, quotations for recent similar works and soft market testing. Soft market testing has been conducted with potential suppliers of plant and equipment.

To develop an accurate estimate of the heat network costs, the proposed network has been broken down into constituent parts (i.e. straight pipe lengths, pipe bends, valves, valve chambers, welds, weld inspections, etc.) for each pipe section. These quantities have then been multiplied by the average rates taken from numerous quotations obtained for similar work. A complexity factor has been added to this to account for the areas of lower implementation or construction complexity and areas of higher complexity such as main roads, key intersections and areas of congested utilities.

Estimated capital costs for key plant items (such as heat pumps, thermal storage tanks, etc.) have been obtained from the respective suppliers.

By using the above methodology, CAPEX estimates are within the tolerance stated in the project requirements and ITT and contingency has been applied to each element of capital expenditure as appropriate.

Capital Costs

Capital costs for the scheme are based on a combination of previous project experience, quotations for recent similar works and soft market testing. Soft market testing has been conducted with potential suppliers of plant and equipment.

A summary of network capital costs is shown i[n Table 50.](#page-125-0)

Table 50: Capital costs

Connection Costs and Connection Charges

It has been assumed the network operator covers costs of all connections with the initial CAPEX investment. Any future planned developments would be required to pay a connection charge which would cover the costs of connecting to the network. The maximum connection charge would be based on the avoided cost of an equivalent low carbon heating solution (e.g. ASHPs) The cost of this would need to be agreed with each future commercial connection. Connection charges for domestic planned developments would also be based on the avoided costs of installing individual ASHPs. These have been included in the base case assessment at £8,125/dwelling.

Network costs

Network costs are shown below i[n Table 51,](#page-127-0) [Table 52,](#page-127-1) [Table 53](#page-128-0) an[d Table 54.](#page-128-1)

Table 51: Network spine costs not cumulative (not including contingency)

Table 52: Network connection costs – Phase 1

Table 53: Network connection costs - Phase 2

Table 54: Network connections costs – Phase 3

APPENDIX 7: BUILDLING CONNECTIONS – EXISTING HEATING SYSTEMS

[Table 55](#page-129-0) an[d Table 56](#page-129-1) show examples for potential improvement measures for existing heating systems and hot water systems respectively.

Table 55: Types of heating system

Table 56: Types of hot water system

APPENDIX 8: HEAT PUMP REFRIGERANT

There are advantages and disadvantages associated with different refrigerants and the choice of refrigerant in heat pumps can depend on a number of criteria including efficiency, required water temperatures and scale.

Most domestic scale heat pumps use synthetic refrigerants (HFCs) that have a high Global Warming Potential (GWP) meaning they have a considerable environmental impact when they leak. This impact can be two to three thousand times higher than CO2. For this reason, the UK has committed to the Kigali amendment of the Montreal Protocol in January 2019 where we commit to cutting the production and consumption of HFCs by more than 80% over the next 30 years and replacing them with less damaging, ideally natural, alternatives.

The European Commission F-gas phase down states that by 2021-2023 the average GWP of refrigerants should be less than 900, and by 2030 the average GWP should be 400. The lifetime of chilling or heating plant is approximately 15-20 years. Therefore, plant installed now will require a GWP of less than 400, as otherwise by 2030, it will exceed the Kilgali Amendment phase down targets. Net zero CO₂e targets will also be affected by plant and equipment installed in buildings that contain powerful greenhouse gases. All new buildings should consider the lifetime impacts of the refrigerant as well as efficiency to reduce overall emissions of greenhouse gases.

The main refrigerants used in commercially available heat pumps are summarised in [Table 57](#page-130-0) below:

Table 57: Refrigerants used in heat pump systems

